

MAX17662

3.5V to 36V, 2A, High-Efficiency, Synchronous Step-Down DC-DC Converter

General Description

The Himalaya series of voltage regulator ICs, power modules, and chargers enables cooler, smaller, and simpler power supply solutions. The MAX17662 is a high-efficiency, Himalaya synchronous step-down DC-DC converter with integrated MOSFETs operating over an input-voltage range of 3.5V to 36V. It can deliver up to 2A current. Output voltage is programmable from 0.6V up to 90% of V_{IN} . Built-in compensation across the output-voltage range eliminates the need for external compensation components.

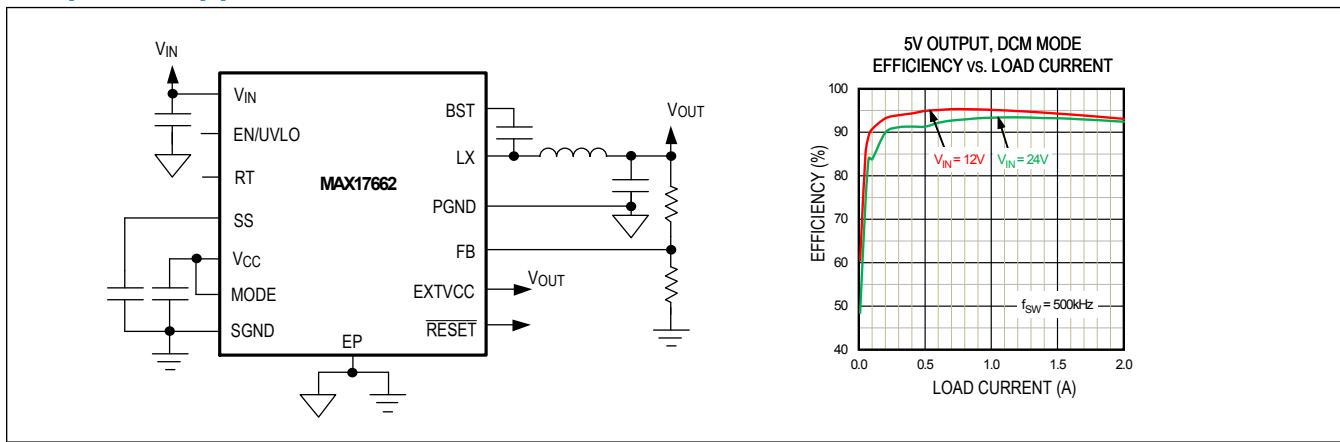
The MAX17662 features a peak-current-mode control architecture. The MAX17662 can be operated in forced pulse-width modulation (PWM), or discontinuous-conduction mode (DCM) to enable high efficiency under full-load and light-load conditions. The MAX17662 offers a low minimum on-time that allows high switching frequencies and a smaller solution size.

The feedback-voltage regulation accuracy over -40°C to $+125^{\circ}\text{C}$ is $\pm 1.33\%$. The device is available in a 16-pin (3mm x 3mm) TQFN-EP package. Simulation models are available.

Applications

- Industrial Control Power Supplies
- General-Purpose Point-of-Load
- Distributed Supply Regulation
- Base Station Power Supplies
- Wall Transformer Regulation
- High-Voltage, Single-Board Systems

Simplified Application Circuit



www.datasheetall.com

[Ordering Information](#) appears at end of data sheet.

19-100525; Rev 1; 6/21

Absolute Maximum Ratings

V _{IN} to PGND.....	-0.3V to +40V	LX total RMS current.....	±3.8A
EN/UVLO to SGND.....	-0.3V to +40V	Output Short-Circuit duration.....	Continuous
LX to PGND.....	-0.3V to (V _{IN} + 0.3V)	Continuous Power Dissipation (T _A = +70°C)	
EXTVCC to SGND.....	-0.3V to +14V	TQFN Multilayer Board (derate 23.1mW/°C above +70°C).....	1847.6mW
BST to PGND.....	-0.3V to +42V	Operating Temperature Range (Note 1).....	-40°C to +125°C
BST to LX.....	-0.3V to +2.2V	Junction Temperature.....	+150°C
BST to V _{CC}	-0.3V to +40V	Storage Temperature Range.....	-65°C to +150°C
FB, V _{CC} to SGND.....	-0.3V to +2.2V	Lead Temperature (soldering, 10s).....	+300°C
SS, RT to SGND.....	-0.3V to (V _{CC} + 0.3V)	Soldering Temperature (reflow).....	+260°C
MODE, RESET to SGND.....	-0.3V to +6V		
PGND to SGND.....	-0.3V to +0.3V		

Note 1: Junction temperature greater than +125°C degrades operating lifetimes.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Package Information

16 TQFN-EP

Package Code	T1633+5C
Outline Number	21-0136
Land Pattern Number	90-0032
Thermal Resistance, Four-Layer Board (Note 2)	
Junction-to-Ambient (θ _{JA})	38°C/W
Junction-to-Case Thermal Resistance (θ _{JC})	4°C/W

For the latest package outline information and land patterns (footprints), go to www.maximintegrated.com/packages. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

Note 2: Package thermal resistances were obtained using the MAX17662 Evaluation Kit with no airflow.

Electrical Characteristics

($V_{IN} = V_{EN/UVLO} = 24V$, $RT = \text{Unconnected}$ ($f_{SW} = 500\text{kHz}$), $C_{VCC} = 2.2\mu\text{F}$, $V_{MODE} = V_{EXTVCC} = V_{SGND} = V_{PGND} = 0$, $V_{FB} = 0.64V$, $LX = SS = \text{RESET} = \text{Open}$, V_{BST} to $V_{LX} = 1.8V$, $T_A = T_J = -40^\circ\text{C}$ to 125°C , unless otherwise noted. Typical values are at $T_A = +25^\circ\text{C}$. All voltages are referenced to SGND, unless otherwise noted. (Note 3))

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
INPUT SUPPLY (V_{IN})						
Input Voltage Range	V_{IN}		3.5	36		V
Input Shutdown Current	I_{IN_SH}	$V_{EN/UVLO} = 0V$ (Shutdown mode)	6.5	24		μA
Input Quiescent Current	I_{Q_DCM}	DCM mode, $V_{LX} = 0.1V$	2			mA
	I_{Q_PWM}	Normal Switching mode, $V_{FB} = 0.58V$	8.2			
Input UVLO	$V_{IN_UVLO_R}$	V_{IN} rising	2.95	3.26		V
	V_{IN_HYS}	Hysteresis	0.246			
ENABLE/INPUT UNDERVOLTAGE LOCKOUT (EN/UVLO)						
EN/UVLO Threshold	V_{ENR}	$V_{EN/UVLO}$ rising	1.194	1.25	1.303	V
	V_{EN_HYS}	Hysteresis	0.1			
	V_{EN_TRUESD}	$V_{EN/UVLO}$ falling, true shutdown	0.75			
EN/UVLO Input Leakage Current	I_{EN}	$V_{EN/UVLO} = 0V$, $T_A = +25^\circ\text{C}$	-50	0	+50	nA
LINEAR REGULATOR (V_{CC}, $EXTVCC$)						
V _{CC} Output Voltage Range	V_{CC}	3.5V < V_{IN} < 36V, $I_{VCC} = 1\text{mA}$	1.74	1.80	1.86	V
		1mA < I_{VCC} < 25mA	1.70	1.80	1.86	
V _{CC} UVLO	V_{CC_UVR}	V_{CC} rising	1.605	1.640	1.683	V
		Hysteresis	0.065			
EXTVCC Operating Voltage Range			2.448	12		V
EXTVCC Switchover Threshold		EXTVCC rising	2.348	2.400	2.448	V
		Hysteresis	0.09			
EXTVCC Shutdown Current		$V_{EN/UVLO} = 0$, $EXTVCC = 12V$		19		μA
POWER MOSFETS						
High-Side nMOS On-Resistance	R_{DS_ONH}	$I_{LX} = 0.3\text{A}$, sourcing	130	250		$\text{m}\Omega$
Low-Side nMOS On-Resistance	R_{DS_ONL}	$I_{LX} = 0.3\text{A}$, sinking	90	170		$\text{m}\Omega$
LX Leakage Current	I_{LX_LKG}	$V_{IN} = 36V$, $T_A = +25^\circ\text{C}$, $V_{LX} = (V_{PGND} + 1)V$ to $(V_{IN} - 1)V$, $V_{EN/UVLO} = 0V$	-2	+2		μA
SOFT-START (SS)						
Charging Current	I_{SS}	$V_{SS} = 0.3V$	4.7	5	5.3	μA
FEEDBACK (FB)						
FB Regulation Voltage	V_{FB_REG}	$V_{MODE} = V_{SGND}$ (PWM Mode)	0.592	0.600	0.608	V
		$V_{MODE} = V_{CC}$ (DCM Mode)	0.592	0.600	0.608	
FB Input Bias Current	I_{FB}	$V_{FB} = 1V$, $T_A = +25^\circ\text{C}$	-50		+50	nA
MODE SELECTION (MODE)						
MODE Threshold	V_{M_DCM}	DCM mode	1.22			V
	V_{M_PWM}	PWM mode			0.66	

Electrical Characteristics (continued)

($V_{IN} = V_{EN/UVLO} = 24V$, $RT = \text{Unconnected}$ ($f_{SW} = 500\text{kHz}$), $C_{VCC} = 2.2\mu\text{F}$, $V_{MODE} = V_{EXTVCC} = V_{SGND} = V_{PGND} = 0$, $V_{FB} = 0.64V$, $L_X = SS = \text{RESET} = \text{Open}$, V_{BST} to $V_{LX} = 1.8V$, $T_A = T_J = -40^\circ\text{C}$ to 125°C , unless otherwise noted. Typical values are at $T_A = +25^\circ\text{C}$. All voltages are referenced to SGND, unless otherwise noted. (Note 3))

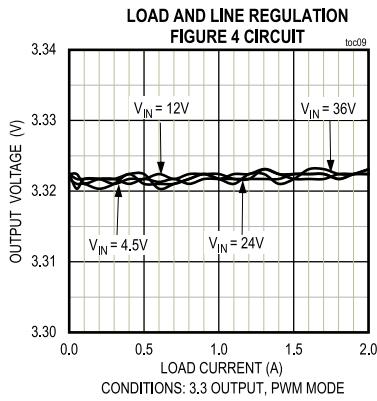
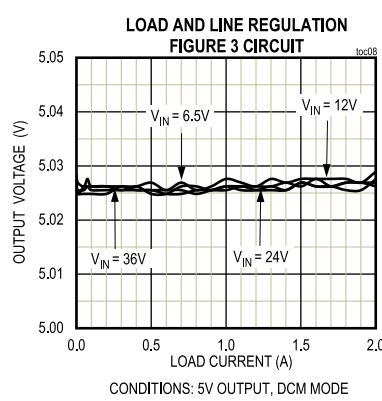
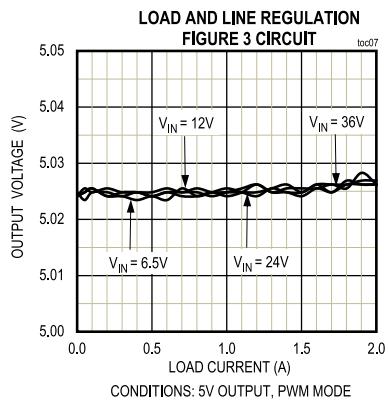
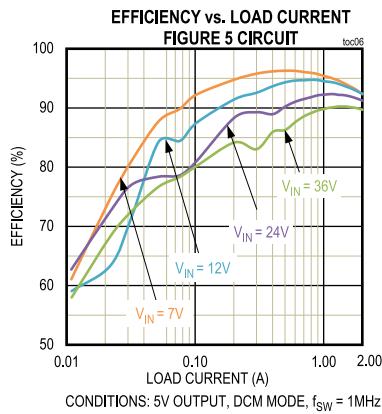
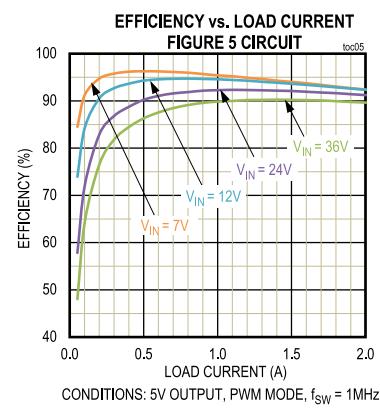
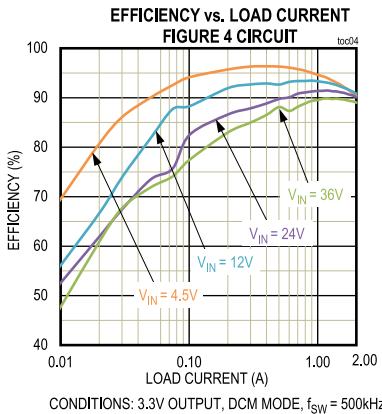
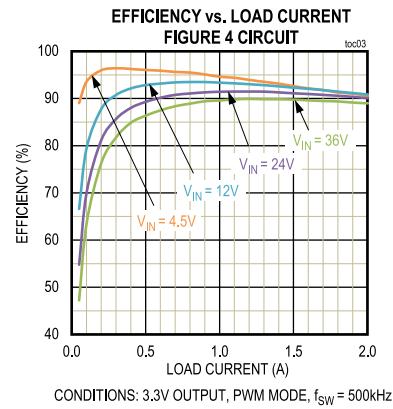
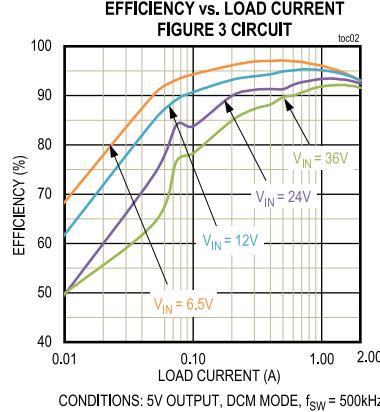
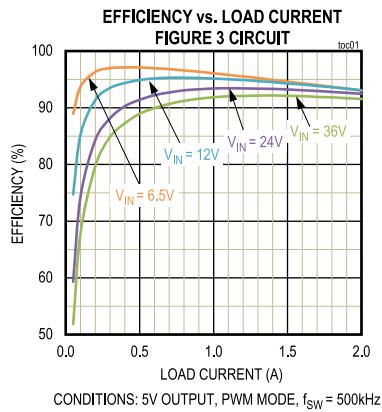
PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
CURRENT LIMIT						
Peak Current-Limit Threshold	I_{PEAK_LIMIT}		2.8	3.4	4.1	A
Valley Current-Limit Threshold	I_{VALLEY_LIMIT}	DCM Mode	0.07	0.22		A
		PWM Mode		-1.8		
OSCILLATOR (RT)						
Switching Frequency	f_{SW}	$R_{RT} = 51.1\text{k}\Omega$	375	400	425	kHz
		$R_{RT} = 8.25\text{k}\Omega$	1980	2200	2420	
		$R_{RT} = \text{Open}$	475	500	525	
V_{FB} Undervoltage Trip Level to Cause Hiccup	V_{FB_HICF}		0.375	0.390	0.405	V
HICCUP Timeout		(Note 4)		32768		Cycles
Minimum On-Time	t_{ON_MIN}			60	90	ns
Minimum Off-Time	t_{OFF_MIN}		100		150	ns
OUTPUT STATUS MONITORING (RESET)						
RESET Output Level Low	V_{RESETL}	$I_{RESET} = 10\text{mA}$		0.4		V
RESET Output Leakage Current	$I_{RESETLKG}$	$T_A = T_J = +25^\circ\text{C}$	-0.1		+0.1	μA
FB Threshold for RESET Deassertion	V_{FB_OKR}	V_{FB} rising	93.1	95.0	97.0	% of V_{FB_REG}
FB Threshold for RESET Assertion	V_{FB_OKF}	V_{FB} falling	89.8	92.0	93.2	% of V_{FB_REG}
RESET Delay After FB Reaches 95% Regulation				1024		Cycles
THERMAL SHUTDOWN						
Thermal-Shutdown Threshold		Temperature rising		160		$^\circ\text{C}$
Thermal-Shutdown Hysteresis				20		$^\circ\text{C}$

Note 3: Electrical specifications are production tested at $T_A = +25^\circ\text{C}$. Specifications over the entire operating temperature range are guaranteed by design and characterization.

Note 4: See [Overcurrent Protection/Hiccup Mode](#) section for more details.

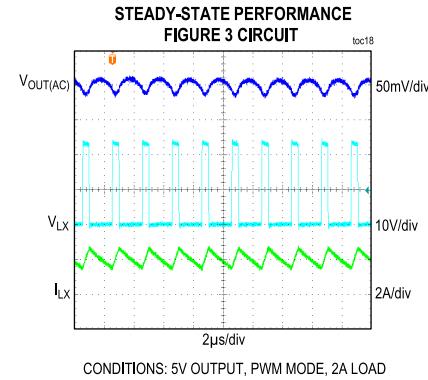
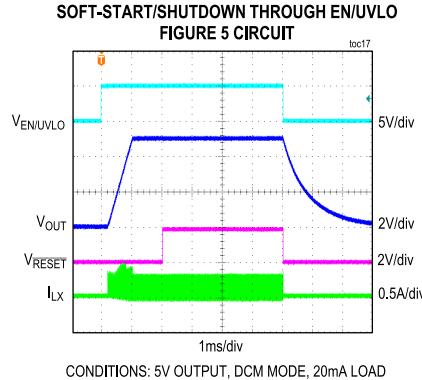
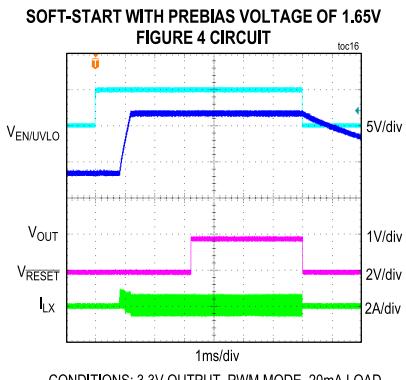
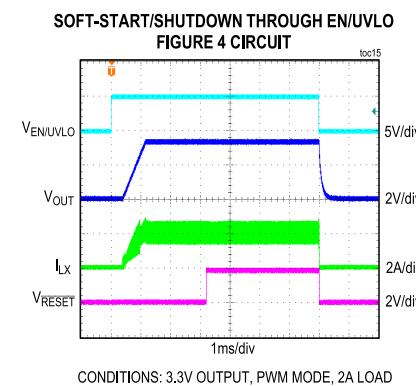
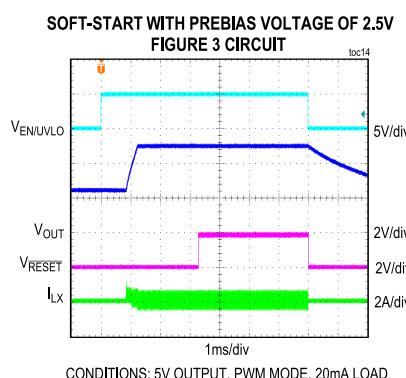
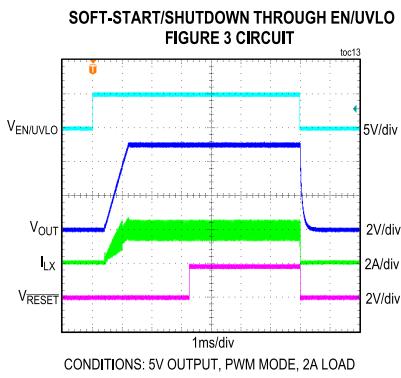
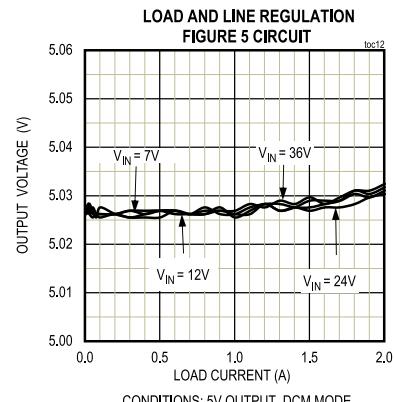
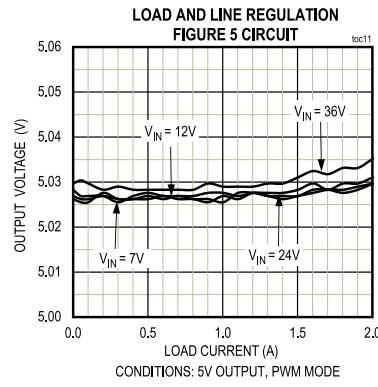
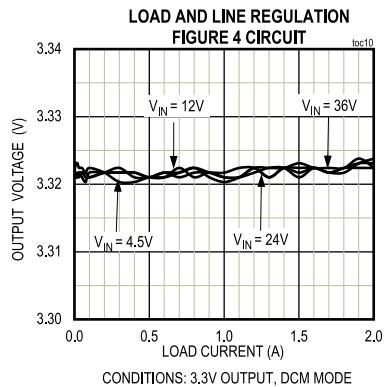
Typical Operating Characteristics

(($V_{EN/UVLO} = V_{IN} = 24V$, $V_{SGND} = V_{PGND} = 0V$, $C_{VCC} = 2.2\mu F$, $C_{BST} = 0.1\mu F$, $C_{SS} = 6800pF$, $T_A = -40^{\circ}C$ to $+125^{\circ}C$, unless otherwise noted. Typical values are at $T_A = +25^{\circ}C$. All voltages are referenced to SGND, unless otherwise noted.))



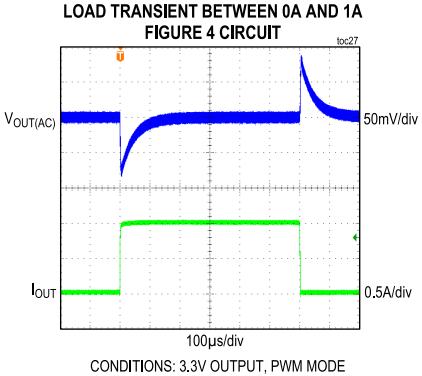
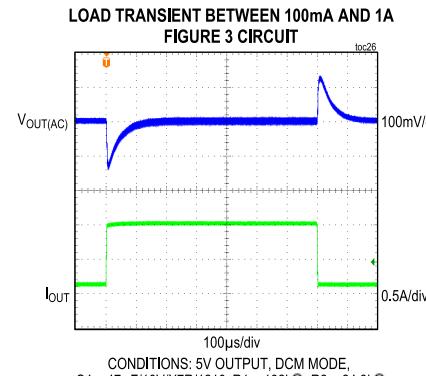
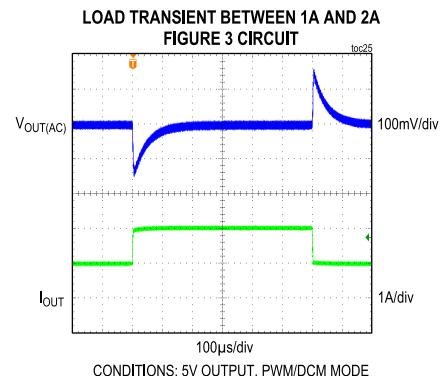
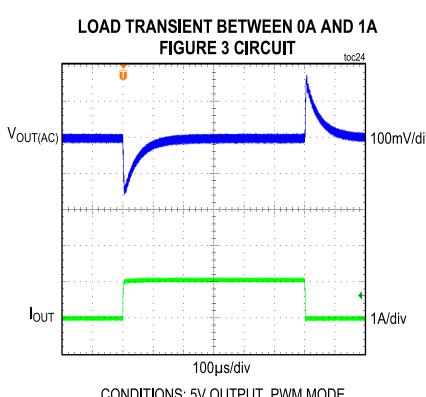
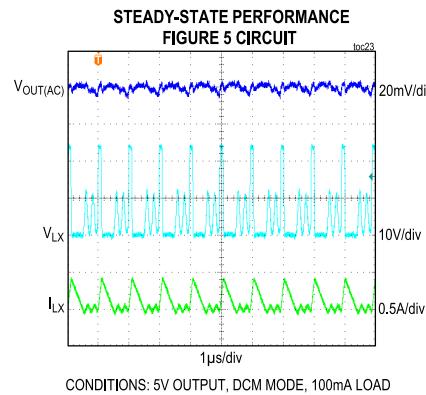
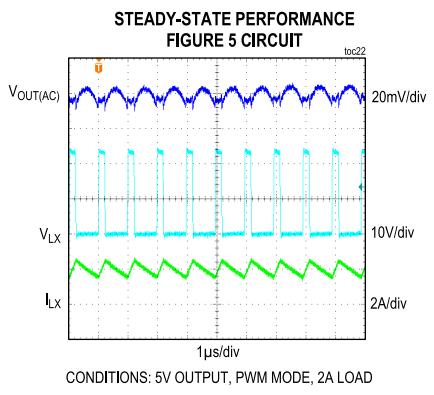
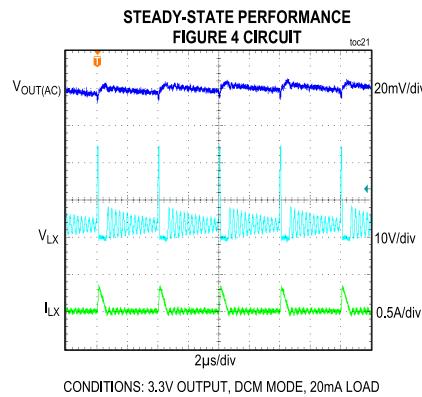
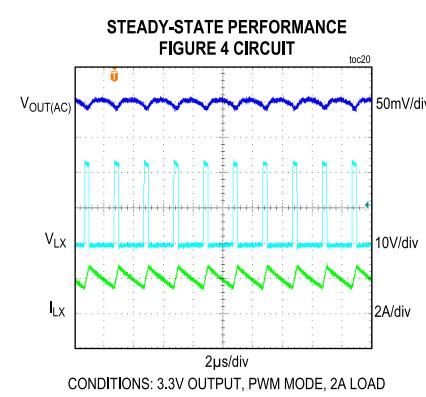
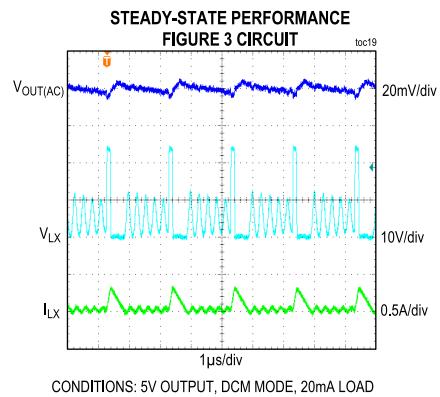
Typical Operating Characteristics (continued)

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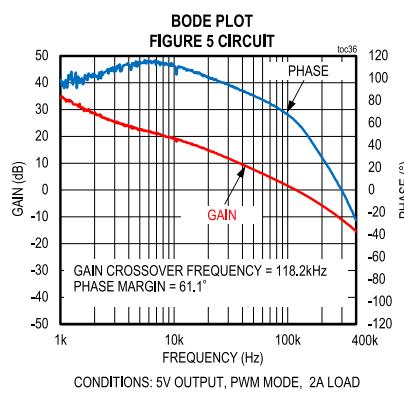
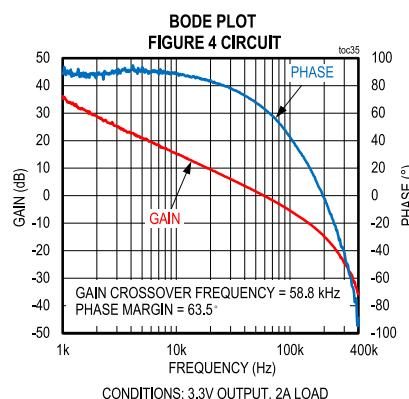
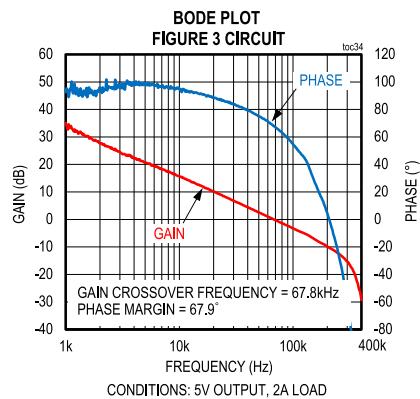
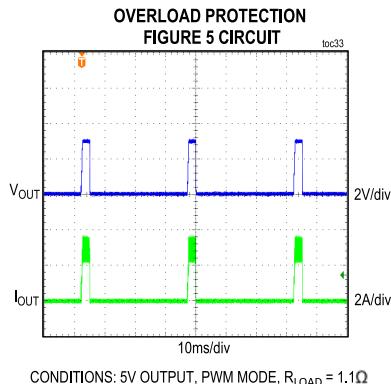
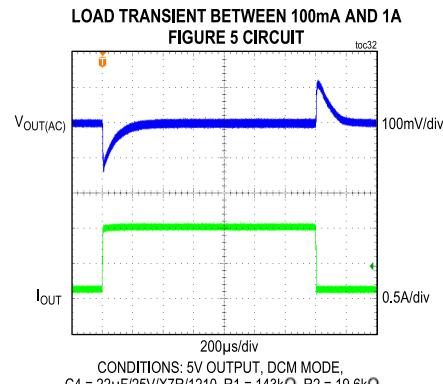
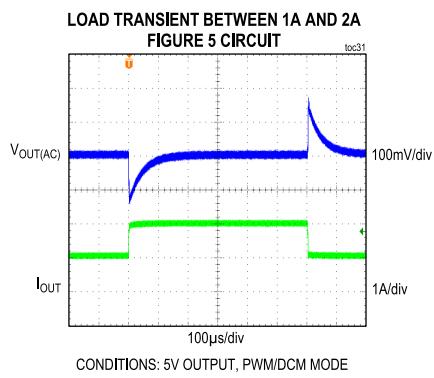
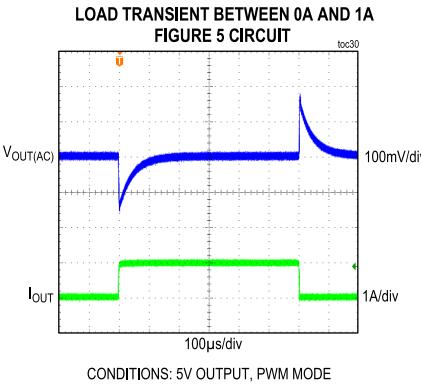
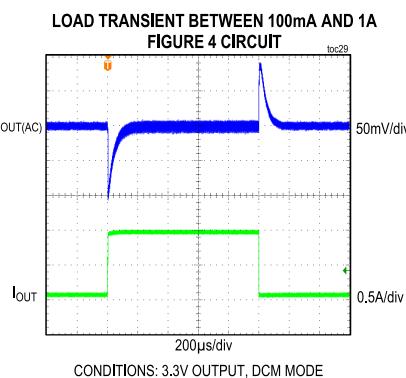
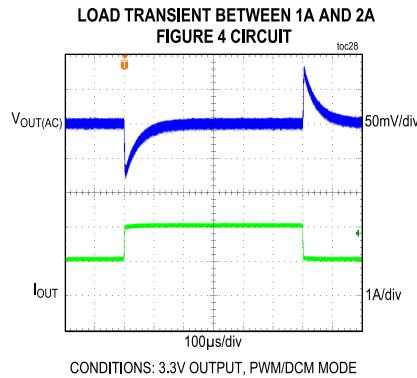
Typical Operating Characteristics (continued)

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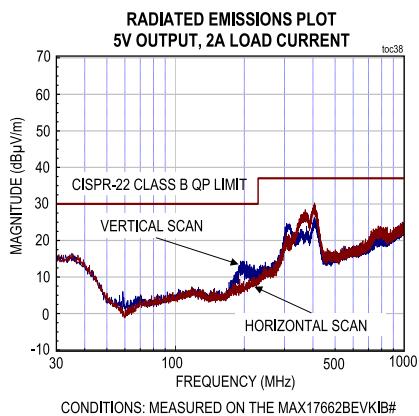
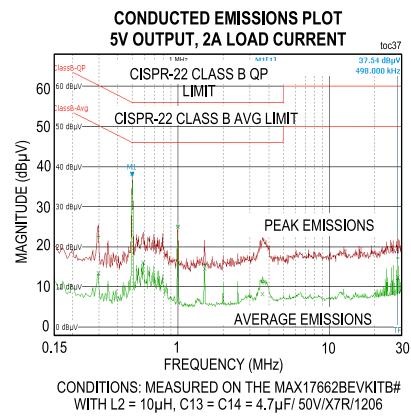
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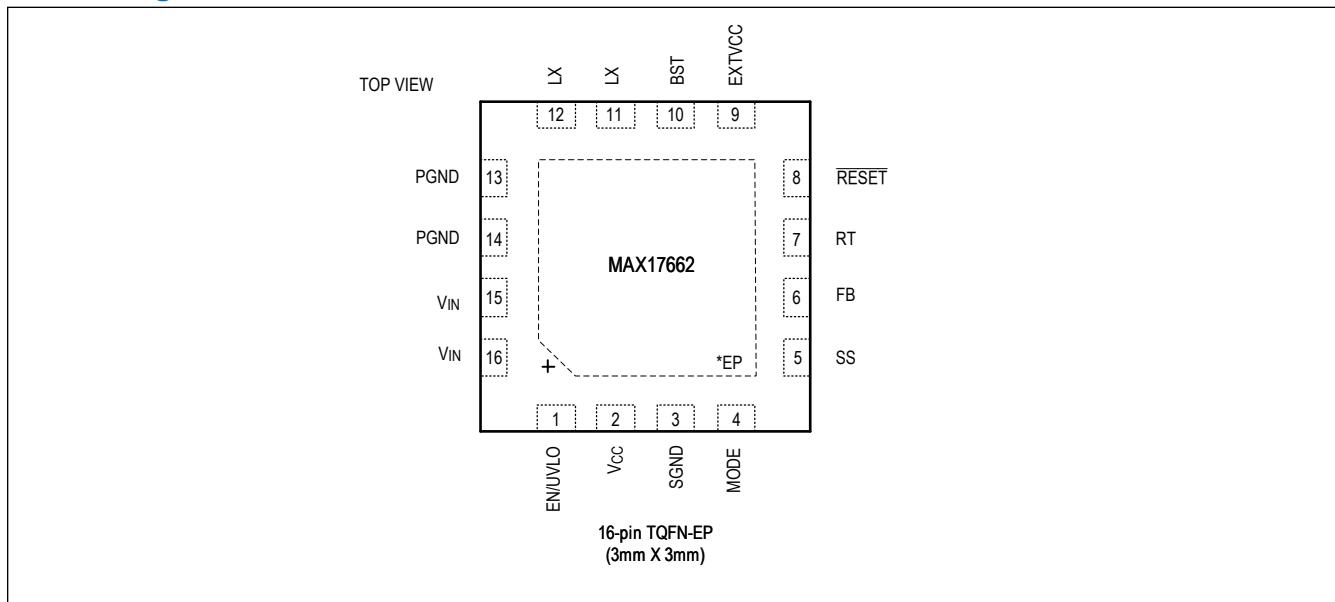


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Pin Configuration



Pin Description

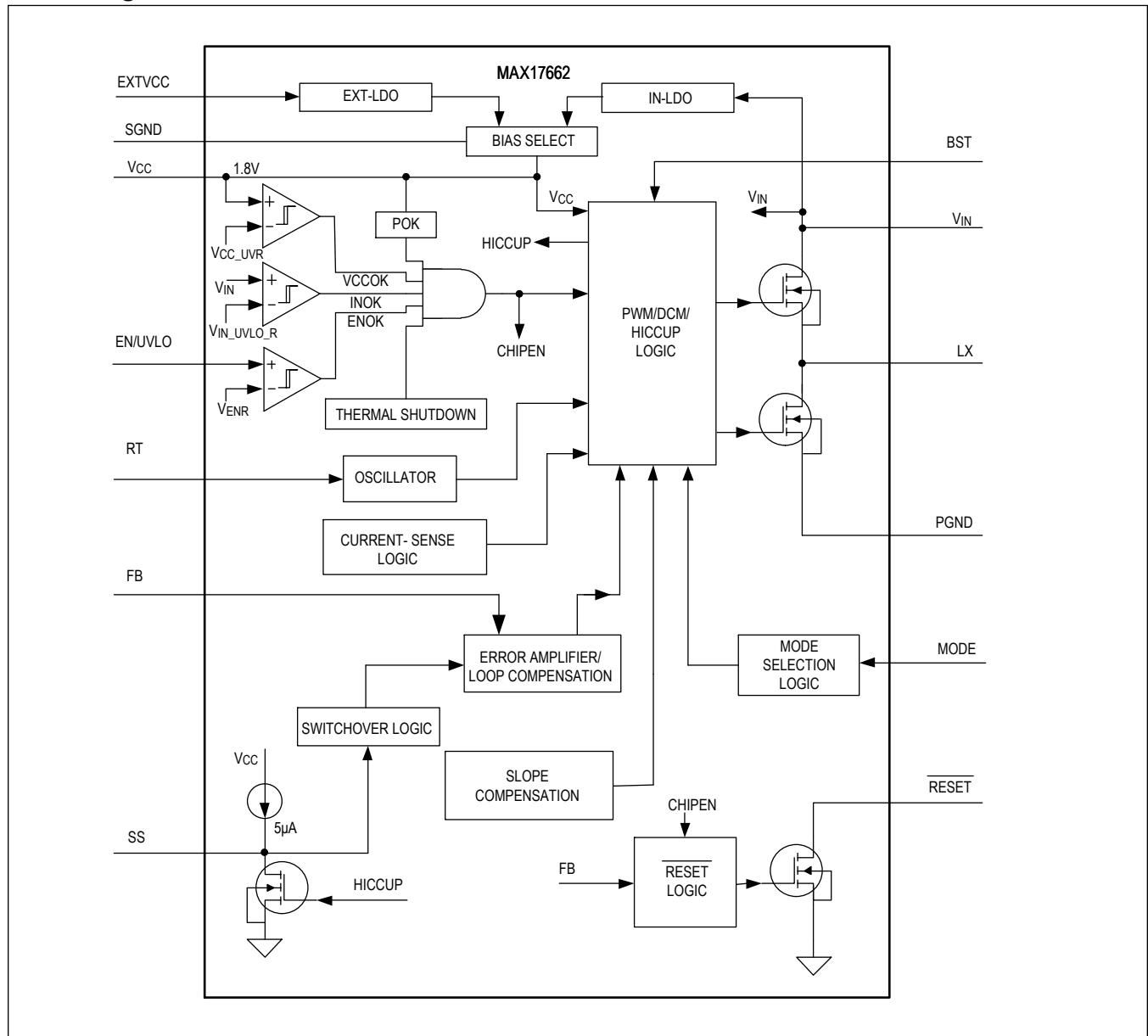
PIN	NAME	FUNCTION
1	EN/UVLO	Enable/Undervoltage Lockout Pin. Drive EN/UVLO high to enable the output. Connect to the center of the resistor-divider between V _{IN} and SGND to set the input voltage at which the part turns on. Connect to V _{IN} pins for always-on operation. Pull low (lower than V _{EN_TRUESD}) for disabling the device.
2	V _{CC}	1.8V LDO Output. Bypass V _{CC} with a 2.2 μ F ceramic capacitance to SGND. LDO does not support the external loading on V _{CC}
3	SGND	Signal Ground
4	MODE	The MODE pin configures the device to operate in either PWM or DCM modes of operation. Connect MODE to SGND for constant-frequency PWM operation at all loads. Connect MODE to V _{CC} for DCM operation (at light loads). See the Mode Selection (MODE) section for more details.
5	SS	Soft-Start Input. Connect a capacitor from SS to SGND to set the soft-start time.
6	FB	Feedback Input. Connect FB to the center node of an external resistor-divider from the output to SGND to set the output voltage. See the Adjusting Output Voltage section for more details.
7	RT	Programmable Switching Frequency Input. Connect a resistor from RT to SGND to set the regulator's switching frequency between 400kHz and 2.2MHz. Leave RT pin open for the default 500kHz frequency. See the Setting the Switching Frequency (RT) section for more details.
8	RESET	Open-Drain RESET Output. The RESET output is driven low if FB drops below V _{FB_OKF} . RESET goes high 1024 cycles after FB rises above V _{FB_OKR} .
9	EXTVCC	External Bias Input. Applying a voltage between 2.448V and 12V at EXTVCC will bypass the IN-LDO and improve overall converter efficiency. Connect a buck regulator output to EXTVCC through an RC filter (4.7 Ω , 0.1 μ F) to protect the EXTVCC pin from reaching its absolute maximum rating (-0.3V) during an output short-circuit condition. When EXTVCC is not used, connect it to SGND.
10	BST	Bootstrap Capacitor. Connect a 0.1 μ F ceramic capacitor between BST and LX.
11, 12	LX	Switching Node Pins. Connect LX pins to the switching side of the inductor.

Pin Description (continued)

PIN	NAME	FUNCTION
13, 14	PGND	Power Ground Pins of the Converter. Connect externally to the power ground plane. Refer to the MAX17662 Evaluation Kit data sheet for a layout example.
15, 16	V _{IN}	Power-Supply Input Pins. 3.5V to 36V input-supply range. Decouple to PGND with a minimum 2.2 μ F capacitor; place the capacitor close to the V _{IN} and PGND pins. See Input Capacitor Selection for more details.
—	EP	Exposed Pad. Always connect EP to the SGND pin of the IC. Also, connect EP to a large plane with several thermal vias for best thermal performance. Refer to the MAX17662 Evaluation Kit data sheet for an example of the correct method for EP connection and thermal vias.

Block Diagram

Block Diagram



Detailed Description

The MAX17662 is a high-efficiency, synchronous step-down DC-DC converter with integrated MOSFETs. It can deliver up to 2A over an input voltage range of 3.5V to 36V. Built-in compensation across the output-voltage range eliminates the need for external compensation components. The feedback-voltage regulation accuracy over -40°C to $+125^{\circ}\text{C}$ is $\pm 1.33\%$.

The device features a peak-current-mode control architecture. An internal transconductance error amplifier produces an integrated error voltage at an internal node, which sets the duty cycle using a PWM comparator, a high-side current-sense amplifier, and a slope-compensation generator. At each rising edge of the clock, the high-side MOSFET turns on and remains on until either the appropriate or maximum duty cycle is reached, or the peak current limit is detected. During the high-side MOSFET's on-time, the inductor current ramps up. During the second half of the switching cycle, the high-side MOSFET turns off and the low-side MOSFET turns on. The inductor releases the stored energy as its current ramps down and provides current to the output.

The device features a MODE pin that can be used to operate the device in PWM or DCM mode. The device also features adjustable-input undervoltage lockout, adjustable soft-start, and output voltage monitoring with open-drain RESET. The MAX17662 offers a low minimum on time that allows high switching frequencies and a smaller solution size.

Mode Selection (MODE)

The MAX17662 supports forced PWM and DCM mode of operation. The device enters the required mode of operation based on the setting of the MODE pin as detected during power-up after V_{IN} , V_{CC} , and EN/UVLO voltages exceed their respective UVLO rising thresholds ($V_{IN_UVLO_R}$, V_{CC_UVR} , V_{ENR}). If the state of the MODE pin is high ($> V_{M_DCM}$), the device operates in DCM mode at light loads. If the state of the MODE pin is low ($< V_{M_PWM}$), the device operates in constant-frequency PWM mode at all loads. See the MODE section in the [Electrical Characteristics](#) table for details.

PWM Mode Operation

In PWM mode, the inductor current is allowed to go negative. PWM operation provides constant frequency operation at all loads and is useful in applications sensitive to switching frequency. However, the PWM mode of operation gives lower efficiency at light loads compared to the DCM mode of operation.

DCM Mode Operation

In DCM mode of operation, the inductor current can be discontinuous at light loads. The inductor current is not allowed to go negative. Switching pulses are skipped when the buck converter is operated close to no-load condition. DCM operation offers better efficiency performance compared to PWM at light loads. The steady-state output voltage ripple in DCM mode is comparable to PWM mode.

Linear Regulator (V_{CC} and $EXTVCC$)

The MAX17662 has two built-in low dropout (LDO) linear regulators that power V_{CC} . One LDO is powered from V_{IN} (IN-LDO), while the other LDO is powered from $EXTVCC$ (EXT LDO). The IN-LDO is enabled either during power-up or when voltage on EN/UVLO pin is recycled. Only one of the two LDOs is in operation at a time, depending on the voltage present at $EXTVCC$. If $EXTVCC$ is greater than 2.4V (typ), V_{CC} is powered by EXT LDO. Powering V_{CC} from $EXTVCC$ increases efficiency at higher input voltages. The typical V_{CC} output voltage is 1.8V. Bypass V_{CC} to SGND with a 2.2 μF low-ESR ceramic capacitor. V_{CC} powers the internal blocks and the low-side MOSFET driver. V_{CC} also recharges the external bootstrap capacitor.

The MAX17662 employs an undervoltage-lockout circuit that forces the buck converter off when V_{CC} falls below the falling threshold ($V_{CC_UVR} - V_{CC_HYS}$). The buck converter can be immediately enabled again when $V_{CC} > V_{CC_UVR}$. The 65mV (typ) UVLO hysteresis prevents chattering on power-up/power-down.

If the buck converter output is shorted to ground in applications where the converter output is connected to the $EXTVCC$ pin, then the transfer from EXT LDO to the IN-LDO happens seamlessly, without any impact to normal functionality. Add a local bypass capacitor of 0.1 μF on the $EXTVCC$ pin to SGND, and a 4.7 Ω resistor from the buck regulator output node to the $EXTVCC$ pin, to protect the $EXTVCC$ pin from reaching its absolute maximum rating (-0.3V) during output short-circuit conditions. Connect $EXTVCC$ pin to SGND when not in use.

Setting the Switching Frequency (RT)

The switching frequency of the device can be programmed between 400kHz and 2.2MHz by using a resistor connected from the RT pin to SGND. The switching frequency (f_{SW}) is related to the resistor connected at the RT pin (R_{RT}) by the following equation:

$$R_{RT} = \frac{20625}{f_{SW}} - 1$$

where, R_{RT} is in kΩ and f_{SW} is in kHz. Leaving the RT pin open makes the device operate at the default switching frequency of 500kHz. See [Table 1](#) for RT resistor values for a few common switching frequencies.

Table 1. Switching Frequency vs. RT Resistor

SWITCHING FREQUENCY (kHz)	RT RESISTOR (kΩ)
400	51.1
500	Open
500	40.2
2200	8.25

Operating Input Voltage Range

The minimum and maximum operating input voltages for a given output voltage setting should be calculated as follows:

$$V_{IN(MIN)} = \frac{V_{OUT} + (I_{OUT(MAX)} \times (R_{DCR(MAX)} + R_{DS_ONL(MAX)}))}{1 - (f_{SW(MAX)} \times t_{OFF_MIN(MAX)})} + (I_{OUT(MAX)} \times (R_{DS_ONH(MAX)} - R_{DS_ONL(MAX)}))$$

$$V_{IN(MAX)} = \frac{V_{OUT}}{f_{SW(MAX)} \times t_{ON_MIN(MAX)}}$$

where:

V_{OUT} = Programmed steady-state output voltage

$I_{OUT(MAX)}$ = Maximum load current

$R_{DCR(MAX)}$ = Worst-case DC resistance of the inductor

$f_{SW(MAX)}$ = Maximum switching frequency

$t_{OFF_MIN(MAX)}$ = Worst-case minimum switch off-time (150ns)

$t_{ON_MIN(MAX)}$ = Worst-case minimum switch on-time (90ns)

$R_{DS_ONL(MAX)}$ and $R_{DS_ONH(MAX)}$ = Worst-case on-state resistances of low-side and high-side internal MOSFETs, respectively.

The maximum slew rate that can be applied on input voltage is 30V/μsec.

Overcurrent Protection (OCP)/Hiccup Mode

The MAX17662 features a robust overcurrent-protection (OCP) scheme that protects the device during overload and output short-circuit conditions.

The OCP scheme protects the device by using a hysteretic current control during startup. The startup time is the sum of the programmed soft-start time and 2048 programmed switching frequency clock cycles. When the inductor current exceeds I_{PEAK_LIMIT} (3.4A (typ)), the high-side MOSFET is turned off and the low-side MOSFET is turned on. After the inductor current falls below $0.85 \times I_{PEAK_LIMIT}$, the low-side MOSFET is turned off and high-side MOSFET is turned on at the next clock rising edge.

In steady state, the device operates in cycle-by-cycle peak current limit that turns off the high-side MOSFET when the inductor current exceeds I_{PEAK_LIMIT} and turns on low-side MOSFET. The low-side switch is turned off and high-side switch is turned on at the next clock rising edge. If the feedback voltage drops below V_{FB_HICF} due to a fault condition any time after startup time is complete, the hiccup mode is triggered.

In hiccup mode, the converter is protected by suspending switching for a hiccup timeout period of 32,768 clock cycles of the programmed switching frequency before soft-start is attempted again. During startup time, if feedback voltage does not exceed V_{FB_HICF} , the device continues to operate in hysteretic control. Hiccup mode of operation ensures low average power dissipation under output short-circuit conditions.

RESET Output

The device includes a RESET comparator to monitor the status of the output voltage. The open-drain RESET output requires an external pullup resistor. RESET goes high (high impedance) 1024 switching cycles after the FB voltage increases above V_{FB_OKR} . RESET goes low when the FB voltage drops to below V_{FB_OKF} . RESET also goes low during thermal shutdown or when the EN/UVLO pin goes below EN/UVLO falling threshold ($V_{ENR} - V_{EN_HYS}$).

Prebiased Output

In a prebiased output condition, both the high-side and the low-side switches are turned off so that the converter does not sink current from the output. High-side and low-side switches do not start switching until the PWM comparator commands the first PWM pulse, at which point switching commences. The output voltage is then smoothly ramped up to the target value in alignment with the internal reference.

Thermal Shutdown Protection

Thermal shutdown protection limits junction temperature of the device. When the junction temperature of the device exceeds $+160^{\circ}\text{C}$, an on-chip thermal sensor shuts down the device, allowing the device to cool. The device turns on with soft-start after the junction temperature reduces by 20°C . Carefully evaluate the total power dissipation (see the [Power Dissipation](#) section) to avoid unwanted triggering of thermal shutdown during normal operation.

Applications Information

Input Capacitor Selection

The input filter capacitor reduces peak currents drawn from the power source and reduces noise and voltage ripple on the input caused by the circuit's switching. The input capacitor RMS current requirement (I_{RMS}) is defined by the following equation:

$$I_{RMS} = I_{OUT(MAX)} \times \frac{\sqrt{V_{OUT} \times (V_{IN} - V_{OUT})}}{V_{IN}}$$

where, $I_{OUT(MAX)}$ is the maximum load current. I_{RMS} has a maximum value when the input voltage equals twice the output voltage ($V_{IN} \approx 2 \times V_{OUT}$), so

$$I_{RMS(MAX)} = \frac{I_{OUT(MAX)}}{2}$$

Choose an input capacitor that exhibits less than $+10^{\circ}\text{C}$ temperature rise at the RMS input current for optimal long-term reliability. Use low-ESR ceramic capacitors with high-ripple-current capability at the input. X7R capacitors are recommended in industrial applications for their temperature stability. Calculate the input capacitance using the following equation:

$$C_{IN} = \frac{I_{OUT(MAX)} \times D \times (1 - D)}{\eta \times f_{SW} \times \Delta V_{IN}}$$

where:

$D = V_{OUT}/V_{IN}$ is the duty ratio of the converter

f_{SW} = switching frequency

ΔV_{IN} = allowable input-voltage ripple

η = efficiency

In applications where the source is located distant from the device input, an appropriate electrolytic capacitor should be added in parallel to the ceramic capacitor to provide necessary damping for potential oscillations caused by the inductance of the longer input power path and input ceramic capacitor.

Inductor Selection

Three key inductor parameters must be specified for operation with the device: inductance value (L), inductor saturation current (I_{SAT}) and DC resistance (R_{DCR}). The switching frequency and output voltage determine the inductor value as follows:

$$L = \frac{V_{OUT}}{1.25 \times f_{SW}}$$

where V_{OUT} and f_{SW} are nominal values and f_{SW} is in Hz. Select an inductor whose value is nearest to the value calculated by the previous formula. Select a low-loss inductor closest to the calculated value with acceptable dimensions and having the lowest possible DC resistance. The saturation current rating (I_{SAT}) of the inductor must be high enough to ensure that saturation can occur only above the peak current-limit value of I_{PEAK_LIMIT} .

Output Capacitor Selection

X7R ceramic output capacitors are preferred due to their stability over temperature in industrial applications. The output capacitors are usually sized to support a step load of 50% of the maximum output current in the application, so output-voltage deviation is contained to 3% of the output-voltage change. The minimum required output capacitance can be calculated as follows:

$$C_{OUT} = \frac{1}{2} \times \frac{I_{STEP} \times t_{RESPONSE}}{\Delta V_{OUT}}$$

$$t_{RESPONSE} \cong \frac{0.33}{f_C}$$

where:

I_{STEP} = Load current step

$t_{RESPONSE}$ = Response time of the controller

ΔV_{OUT} = Allowable output-voltage deviation

f_C = Target closed-loop crossover frequency

f_{SW} = Switching frequency.

Select f_C to be 1/9th of f_{SW} if the switching frequency is less than or equal to 900kHz. If the switching frequency is more than 900kHz, select f_C to be 100kHz. Actual derating of ceramic capacitors with DC-bias voltage must be considered while selecting the output capacitor. Derating curves are available from all major ceramic capacitor manufacturers.

Soft-Start Capacitor Selection

The device implements adjustable soft-start operation to reduce inrush current. A capacitor connected from the SS pin to SGND programs the soft-start time. The selected output capacitance (C_{SEL}) and the output voltage (V_{OUT}) determine the minimum required soft-start capacitor as follows:

$$C_{SS} \geq 28 \times 10^{-6} \times C_{SEL} \times V_{OUT}$$

The soft-start time (t_{SS}) is related to the capacitor connected at SS (C_{SS}) by the following equation:

$$t_{SS} = \frac{C_{SS}}{8.325 \times 10^{-6}}$$

For example, to program a 0.82ms soft-start time, a 6.8nF capacitor should be connected from the SS pin to SGND.

During startup, the device operates at half the programmed switching frequency until the FB pin voltage rises above 0.44V.

Setting the Input Undervoltage-Lockout Level

The device offers an adjustable input undervoltage-lockout level. Set the voltage at which the device turns on with a resistive voltage-divider connected from V_{IN} to SGND (See [Figure 1](#)). Connect the center node of the divider to EN/UVLO. Choose R1 to be $3.3M\Omega$ and then calculate R2 as follows:

$$R2 = \frac{R1 \times 1.25}{(V_{INU} - 1.25)}$$

where V_{INU} is the input-voltage level at which the device is required to turn on. Ensure that V_{INU} is higher than $0.8 \times V_{OUT}$ to avoid hiccup during slow power-up (slower than soft-start)/power-down. If the EN/UVLO pin is driven from an external signal source, a series resistance of minimum $1k\Omega$ is recommended to be placed between the output pin of signal source and the EN/UVLO pin, to reduce voltage ringing on the line.

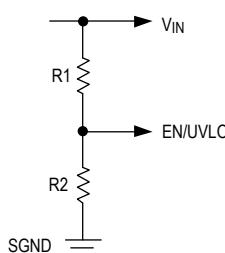


Figure 1. Setting the Input Undervoltage Lockout

Adjusting Output Voltage

The output voltage of the buck converter can be programmed between 0.6V to 90% of V_{IN} . Set the output voltage with a resistive voltage-divider connected from the output-voltage node (V_{OUT}) to SGND (see [Figure 2](#)). Connect the center node of the divider to the FB pin. Use the following procedure to choose the resistive voltage-divider values:

Calculate resistor R_{TOP} from the output to the FB pin as follows:

$$R_{TOP} = \frac{203}{(f_C \times C_{OUT_SEL})}$$

where:

R_{TOP} is in $k\Omega$

f_C = Crossover frequency in Hz

C_{OUT_SEL} = Actual capacitance of selected output capacitor at DC-bias voltage in F.

Calculate resistor R_{BOT} from the FB pin to SGND as follows:

$$R_{BOT} = \frac{R_{TOP} \times 0.6}{(V_{OUT} - 0.6)}$$

R_{BOT} is in $k\Omega$.

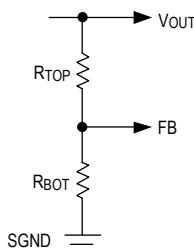


Figure 2. Setting the Output Voltage

Power Dissipation

At a particular operating condition, the power losses that lead to temperature rise of the part are estimated as follows:

$$P_{LOSS} = \left(P_{OUT} \times \left(\frac{1}{\eta} - 1 \right) \right) - (I_{OUT}^2 \times R_{DCR})$$

$$P_{OUT} = V_{OUT} \times I_{OUT}$$

where:

P_{OUT} = Output power

η = Efficiency of the converter

R_{DCR} = DC resistance of the inductor (see the Typical Operating Characteristics for more information on efficiency at typical operating conditions).

For a typical multilayer board, the thermal performance metrics for the package are given below:

$$\theta_{JA} = 38^\circ\text{C/W}$$

$$\theta_{JC} = 4^\circ\text{C/W}$$

The junction temperature of the device can be estimated at any given maximum ambient temperature ($T_{A(MAX)}$) from the following equation:

$$T_{J(MAX)} = T_{A(MAX)} + (\theta_{JA} \times P_{LOSS})$$

If the application has a thermal-management system that ensures that the exposed pad of the device is maintained at a given temperature ($T_{EP(MAX)}$) by using proper heat sinks, then the junction temperature of the device can be estimated at any given maximum ambient temperature as:

$$T_{J(MAX)} = T_{EP(MAX)} + (\theta_{JC} \times P_{LOSS})$$

Note: Junction temperatures greater than $+125^\circ\text{C}$ degrade operating lifetimes.

PCB Layout Guidelines

All connections carrying pulsed currents must be very short and as wide as possible. The inductance of these connections must be kept to an absolute minimum due to the high di/dt of the currents. Since inductance of a current-carrying loop is proportional to the area enclosed by the loop, if the loop area is made very small, inductance is reduced. Additionally, small-current loop areas reduce radiated EMI.

A ceramic input filter capacitor should be placed close to the V_{IN} pins of the IC. This eliminates as much trace inductance effects as possible and gives the IC a cleaner voltage supply. A bypass capacitor for the V_{CC} pin also should be placed close to the pin to reduce effects of trace impedance.

When routing the circuitry around the IC, the signal ground and the power ground for switching currents must be kept separate. They should be connected together at a point where switching activity is minimum. This helps to keep the signal ground quiet. The power ground plane should be kept continuous (unbroken) as far as possible. No trace carrying high switching current should be placed directly over any ground plane discontinuity.

PCB layout also affects the thermal performance of the design. A number of thermal throughputs or vias that connect to a large plane should be provided under the exposed pad of the device for efficient heat dissipation.

For a sample layout that ensures first pass success, refer to the MAX17662 evaluation kit layout available at www.maximintegrated.com.

Typical Application Circuits

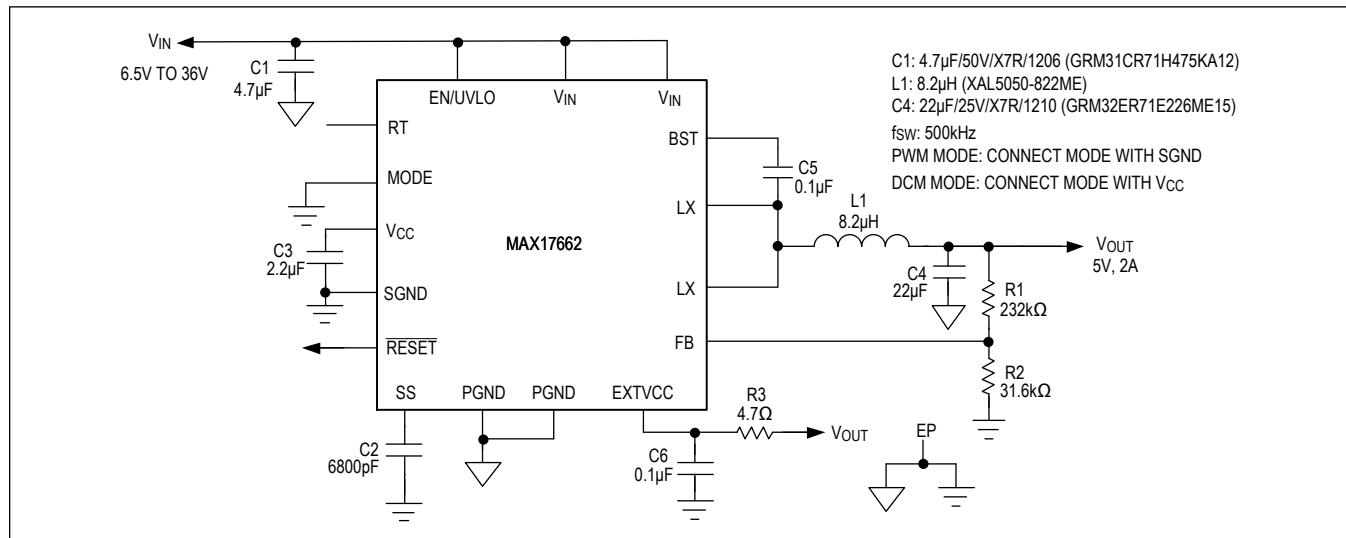


Figure 3. 5V Output with 500kHz Switching Frequency

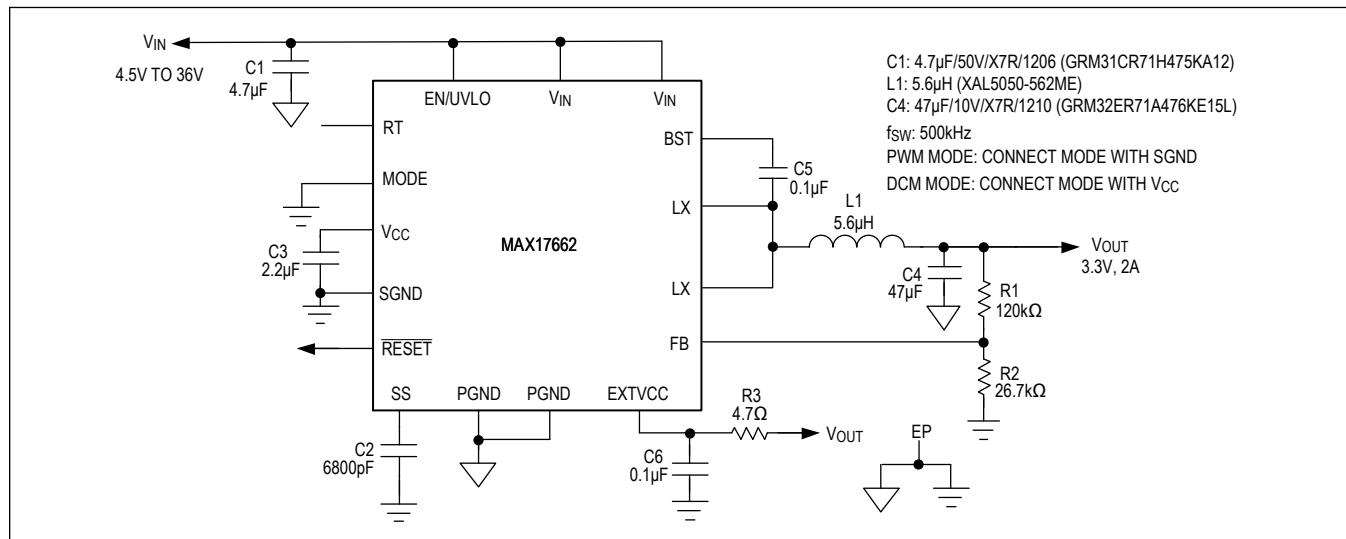


Figure 4. 3.3V Output with 500kHz Switching Frequency

Typical Application Circuits (continued)

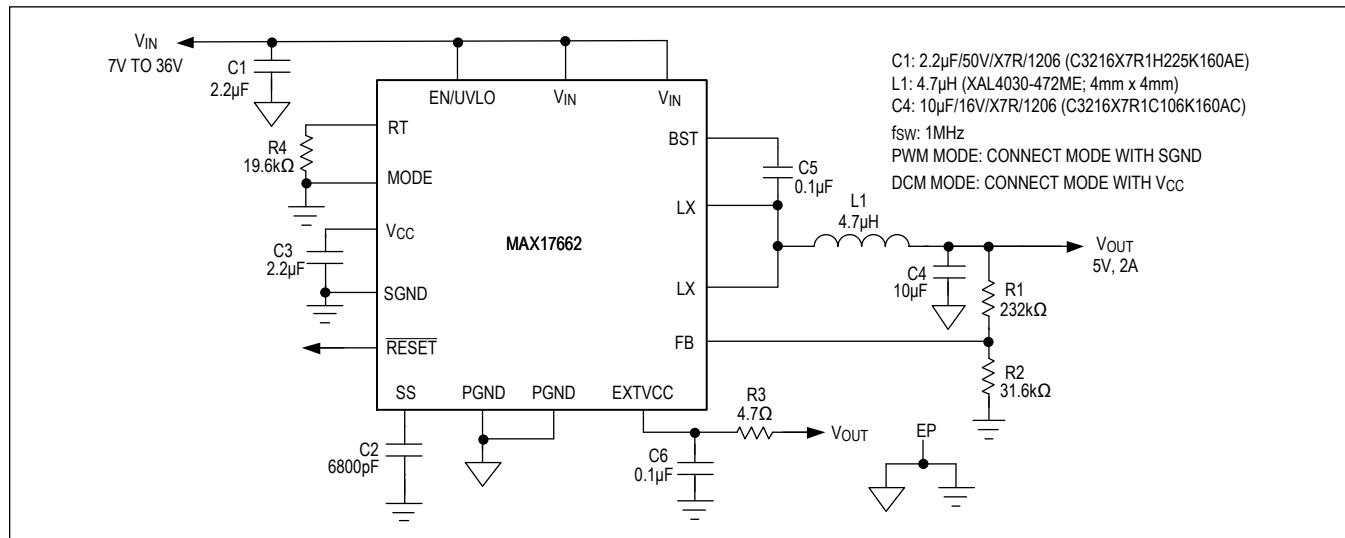


Figure 5. 5V Output with 1MHz Switching Frequency

Ordering Information

PART NUMBER	PIN-PACKAGE
MAX17662BATE+	16 TQFN-EP* (3mmx 3mm)
MAX17662BATE+T	16 TQFN-EP* (3mmx 3mm)

+ Denotes a lead(Pb)-free/RoHS-compliant package.

T = Tape-and-reel.

*EP = Exposed pad.

Revision History

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGES CHANGED
0	7/19	Initial release	—
1	6/21	Updated the <i>General Description</i> , <i>Benefit and Features</i> , <i>Simplified Application Circuit</i> , <i>Absolute Maximum Ratings</i> , <i>Package Information</i> , <i>Electrical Characteristics</i> , <i>Typical Operating Characteristics</i> , <i>Pin Configuration</i> , <i>Pin Description</i> , <i>Block Diagram</i> , <i>Detailed Description</i> , <i>Applications Information</i> , and <i>Typical Application Circuit</i> (Figures 3, 4, and 5) sections	1–6, 10–15, 17–18, 20, 21